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STATIC STABILITY TEST OF THREE ELLIPTIC MISSILE BODY CONFIGURATIONS

Marvin E. Sellers
Calspan Corporation/AEDC Division

SEP6 1985

May 1985

Final Report for Period April 18, 1985

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NOMENCLATURE

Α	Reference	area,	0.18896	ft ²
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AB Base area, 0.18896 ft²

AFA Flow correction angle in pitch, deg

ALPHA Angle of attack, deg

a Semimajor (horizontal) span at X, in.

amax Semimajor span at model base, in. (See Table 1)

BETA Sideslip angle, deg

b Semiminor (vertical) height at X, in.

b_{max} Semiminor height at model base, in. (See Table 1)

CA Forebody axial-force coefficient, body axes, CAT-CAB

CAB Base axial-force coefficient, body axes, -(PBA-P)AB/Q·A

CAT Total axial-force coefficient, body axes, total axial

force/Q-A

CDS Forebody drag coefficient, stability axes

CLL Rolling-moment coefficient, body axes, rolling moment/Q.A.L

CLM Pitching-moment coefficient, body axes, pitching moment/Q.A.L

CLM-AO Slope of CLM versus ALPHA curve at ALPHA = 0, deg^{-1}

CLN Yawing-moment coefficient, body axes, yawing moment/Q.A.L

CLS Forebody lift coefficient, stability axes

CN Normal-force coefficient, body axes, normal force/Q·A

CN-AO Slope of CN versus ALPHA curve at ALPHA = 0, deq^{-1}

CONFIG Model configuration designation

CY Side-force coefficient, body axes, side force/Q.A

Reference length, in. (See Table 1)

(L/D)S Lift-to-drag ratio, stability axes

LM Model length, 36.000 in.

M Free-stream Mach number

NCP Normal-force center-of-pressure location, body axes, inches
from nose; XMRP-(CLM·L/CN) or XMRP-(CLM-AO·L/CN-AO) for ALPHA

P Free-stream static pressure, psfa

PBA Average base pressure, (PBT + PBB + PBL + PBR)/4, psfa

PBi Base pressure, i = T, B, L, and R, where T, B, L, and R are top, bottom, left, and right looking upstream, respectively, psfa

PHI Roll angle, deg

PN Data point number

PT Tunnel-stilling chamber pressure, psfa

Q Free-stream dynamic pressure, psf

RE Free-stream unit Reynolds number. ft⁻¹

RUN Data set identification number

T Free-stream static temperature, °R

TT Tunnel-stilling chamber temperature, °R

X Axial location from nose of model, in.

XMRP Axial distance from model nose to model moment-reference location, 24.000 in.

YCP Side-force center-of-pressure location, body axes, inches from nose. XMRP-(CLN·L/CY)

1.0 INTRODUCTION

The work reported herein was conducted by the Arnold Engineering Development Center (AEDC), Air Force Systems Command (AFSC), under Program Element 62201F, Control Number 2404, at the request of Air Force Wright Aeronautical Laboratories (AFWAL/FIMG), Wright-Patterson AFB, Ohio. The AFWAL/FIMG project manager was Mr. Don Shereda. The results were obtained by Calspan Corporation, AEDC Division, operating contractor for the aerospace flight dynamics testing facilities at the AEDC, AFSC, Arnold Air Force Station, Tennessee. The test was conducted in the Aerodynamic Wind Tunnel (4T) of the Propulsion Wind Tunnel (PWT) Facility on April 18, 1985, under AEDC Project Number CD48PB, PWT Test No. TC-793.

The purpose of the test was to obtain data on the aerodynamic characteristics of elliptic missile body configurations with ellipticity ratios of 2.0, 2.5, and 3.0 to 1.0. The test was performed at nominal Mach numbers from 0.4 to 1.3 at a constant nominal free-stream unit Reynolds number of 2.4 million per ft. The angle-of-attack range was -4 to 20 deg at sideslip angles of 0 and 4 deg.

The purpose of this report is to document the test and to describe the test parameters. The report provides information to permit use of the data but does not include any data analysis, which is beyond the scope of this report.

The final data package from the test has been transmitted to AFWAL/FIMG. Request for these data should be addressed to AFWAL/FIMG, Wright-Patterson AFB, OH 45433. A copy of the final tabulated data package is on file on microfilm at the AEDC.

2.0 APPARATUS

2.1 Test Facility

The AEDC Aerodynamic Wind Tunnel (4T) is a closed-loop continuous flow, variable-density tunnel in which the Mach number can be varied from 0.1 to 1.3 and can be set at discrete Mach numbers of 1.6 and 2.0 by placing nozzle inserts over the permanent sonic nozzle. At all Mach numbers, the stagnation pressure can be varied from 300 to 3,400 psfa. The test section is 4-ft square and 12.5 ft long with perforated, variable porosity (0.5- to 10- percent open) walls. It is completely enclosed in a plenum chamber from which air can be evacuated, allowing part of the tunnel airflow to be removed through the perforated walls of the test section. The model support system consists of a sector and sting attachment which has a pitch angle capability of -8 to 27 deg with respect to the tunnel centerline and a roll capability of \pm 180 deg about the sting centerline. A more complete description of the tunnel may be found in Ref. 1.

2.2 Test Articles

The installation of the test articles in Tunnel 4T is shown in Figure 1. The test articles were elliptic missile body configurations with ellipticity ratios of 2.0, 2.5, and 3.0 to 1.0. The models were power-law bodies with an exponent of 0.5 and had the same longitudinal distribution of cross-sectional area. The semi-major and semiminor axis ordinates were derived from the following equations:

For horizontal projection (semimajor axis)

$$a = \frac{a_{\text{max}}}{r^{0.5}} \cdot x^{0.5}$$

and for vertical projection (semiminor axis)

$$b = \frac{b_{\text{max}}}{r.0.5} \cdot x^{0.5}$$

Details of the models are given in Figure 2 and the model configuration designation is presented in Table 1.

2.3 Test Instrumentation

The aerodynamic forces and moments were measured using an internally-mounted, six-component strain-gage balance. Pressures were measured at the base of the model. The radial location of the pressure orifices are shown in Figure 3. The pressures were measured using 15 PSID pressure transducers which are part of the 4T standard pressure system.

3.0 TEST DESCRIPTION

3.1 Test Conditions and Procedures

Measurements of the model steady-state forces and moments were obtained at Mach numbers from 0.4 to 1.3. The nominal test conditions established during the test are given in Table 2. Tunnel conditions were held constant while varying model attitude. Data were recorded at selected angles using the pitch/roll-pause technique. Data were obtained at angles-of-attack from -4 to 20 deg at sideslip angles of 0 and 4 deg. A test run number summary is presented in Table 3.

3.2 Data Acquisition and Reduction

All steady-state measurements were sequentially recorded by the facility on-line computer system and reduced to the desired final form. The data were then tabulated in the Tunnel 4T control room, recorded on magnetic tape, and transmitted to the AEDC central computer file. The data stored in the central computer file were generally available for plotting and analysis on the PWT Interactive Graphics System within 30 seconds after data acquisition. The immediate availability of the tabulated data permitted continual on-line monitoring of the test results. A typical data plot generated on the PWT Interactive Graphics System is shown in Figure 4.

The model force and moment data were reduced to coefficient form in the body- and stability-axes systems. The model reference area is given in the Nomenclature and the reference lengths are given in Table 1. The moment reference point is shown in Figure 2. The stability-axis system coefficients (CLS and CDS) were calculated using the forebody axial-force coefficient (CA) and the normal force coefficient (CN). The base pressure and its area (given in Nomenclature) were used to calculate the base axial-force.

3.3 Corrections

The aircraft angles of attack and sideslip were corrected for sting deflections caused by aerodynamic loads. The flow angularity (AFA) in the tunnel pitch plane was determined by testing the aircraft model upright and inverted, and the flow angularity corrections were then applied to the data. Corrections for the components of model weight, normally termed static tares, were also accounted for before the measured loads were reduced to coefficient form.

3.4 Uncertainty of Measurements

Uncertainties (combinations of system and random errors) of the basic tunnel parameters, shown in Figure 5, were estimated from repeat calibrations of the instrumentation and from the repeatability and uniformity of the test section flow during tunnel calibration. Uncertainties in the instrumentation systems were estimated from repeat calibration of the systems against secondary standards whose uncertainties are traceable to the National Bureau of Standards calibration equipment. The tunnel parameter and instrument uncertainties, for a 95-percent confidence level, were combined using the Taylor series method of error propagation described in Ref. 2 to determine the uncertainties of the parameters in Table 4.

4.0 DATA PACKAGE PRESENTATION

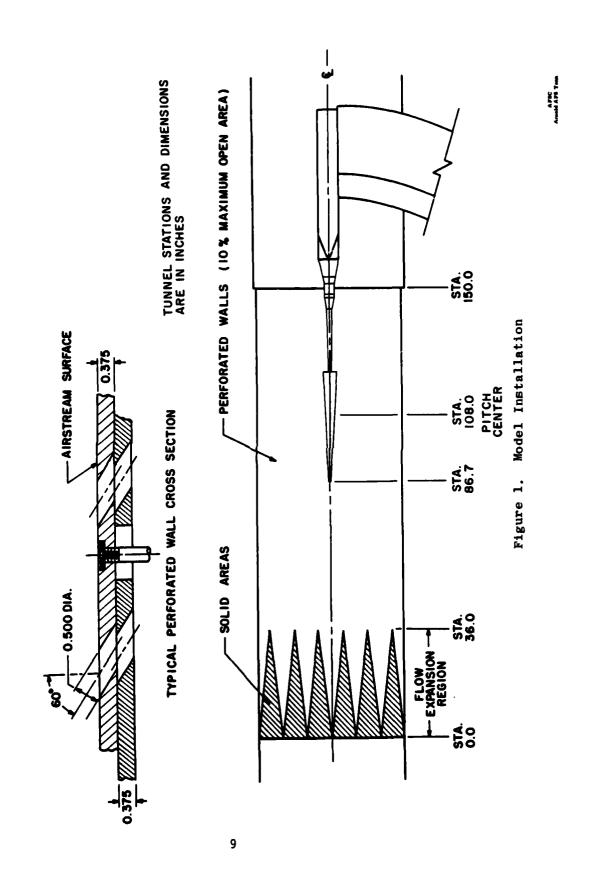
The final data package contained, 1) tabulated data summaries listing specific parameters, 2) digital magnetic computer tapes containing summary data, 3) test article installation photographs, 4) test run number summary, 5) model configuration identification, and 6) model sketches. Sample tabulated data are presented in Appendix III.

5.0 REFERENCES

- 1. <u>Test Facilities Handbook</u> (Twelfth Edition). "Propulsion Wind Tunnel Facility, Vol. 4." Arnold Engineering Development Center, March 1984.
- 2. Abernethy, R.B. and Thompson, J. W., Jr. "Handbook Uncertainty in Gas Turbine Measurements." AEDC-TR-73-5 (AD755356), February 1973.

APPENDIX I

Illustrations



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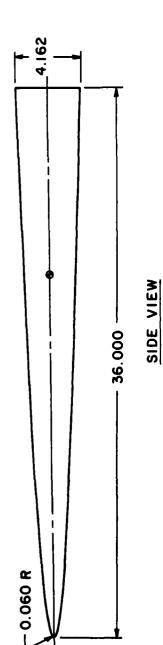
b. Configuration B20 Figure 1. Concluded

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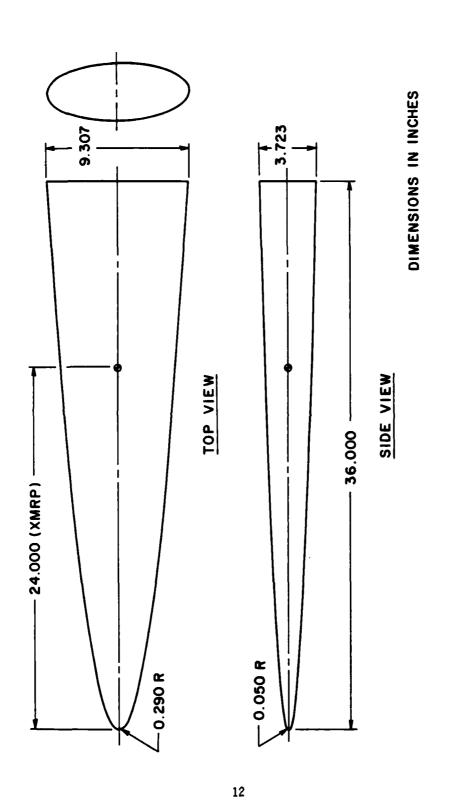
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a. B20 Configuration Figure 2. Model Details

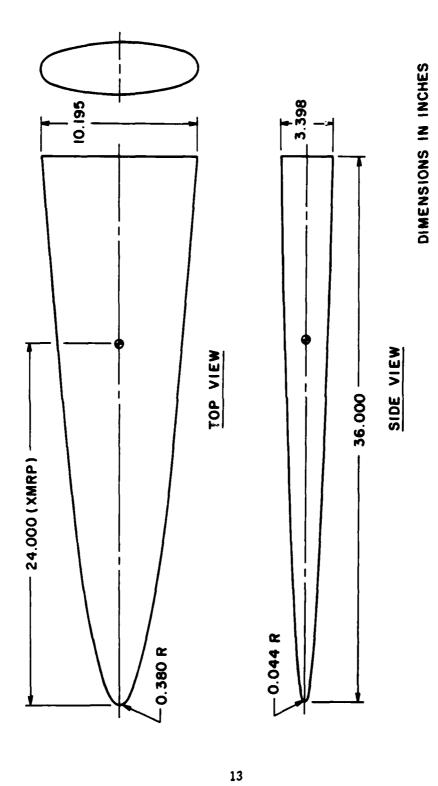
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b. B25 Configuration Figure 2. Continued

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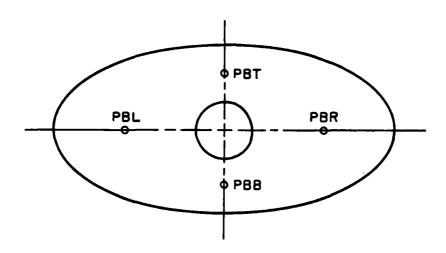


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c. B30 Configuration Figure 2. Concluded

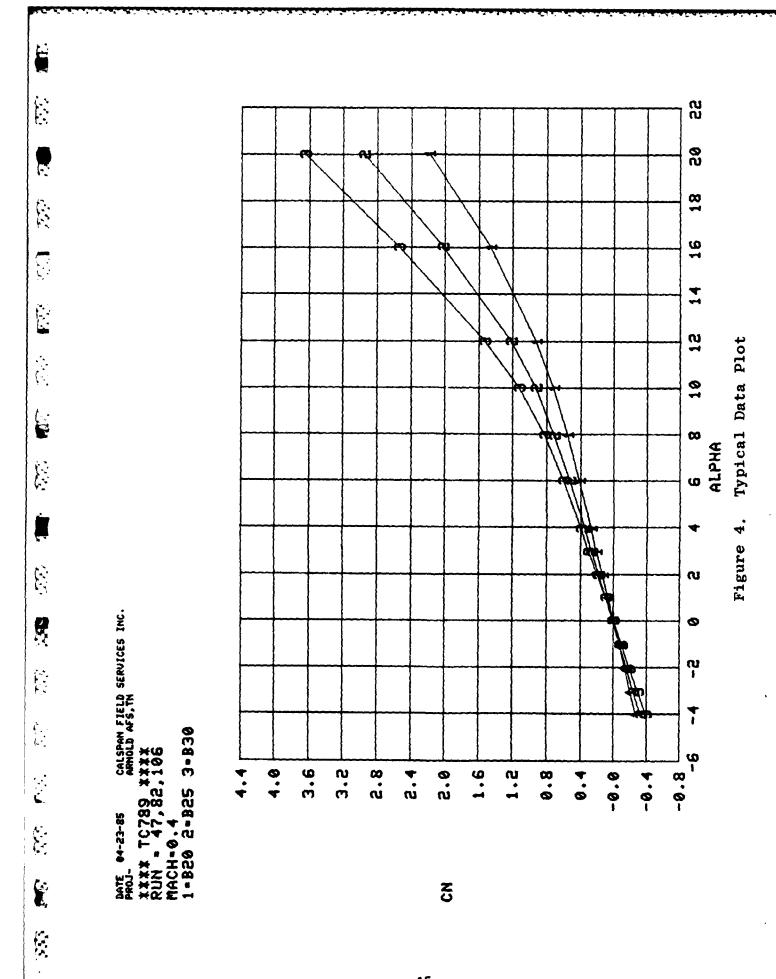


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Looking Upstream (PHI = 0)

Figure 3. Base Pressure Orifice Location



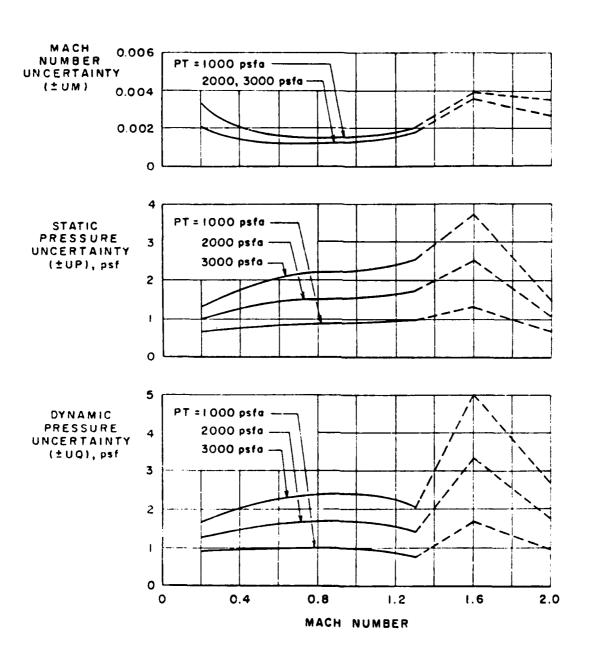


Figure 5. Estimated Uncertainties in 4T Tunnel Parameters

APPENDIX II

Tables

Table 1. Model Configuration Designation

CONFIG	<u>Description</u>
B20	2:1 elliptic body, $a_{max} = 4.162$ in.
	$b_{max} = 2.081 \text{ fm.}$
	L = 8.323 in.
B25	2.5:1 elliptic body, $a_{max} = 4.654$ in.
	b _{max} = 1.862 in.
	L = 9.307 in.
B30	3:1 elliptic body, amax = 5.098 in.
	$b_{max} = 1.699 in.$
	L = 10.195 in.

Table 2. Nominal Test Conditions

М	РТ	Р	Q	RE x 10- 6
0.4	2090	1872	210	2.37
0.55	1625	1324	281	2.40
0.8	1265	829	372	2.41
0.95	1174	659	414	2.39
1.05	1120	584	451	2.46
1.1	1120	524	444	2.36
1.2	1120	462	466	2.38
1.3	1120	405	479	2.37
1.3*	1170	424	500	2.47

^{*} For CONFIG B30 only.

Table 3. Test Run Number Summary

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BETA					Σ				
		0.4	0.55	0.8	0.95	1.05	1.1	1.2	1.3
0		47	90	54	22	09	63	99	20
		72							
4		48	51	55	58	61	64	67	71
0		82	84	86	88	06	92	94	96
4		83	85	87	89	91	93	95	97
0	_	106	108	111	113	115	118	120	122
	-								123
4		107	109	112	114	116	119	121	124

Notes: ALPHA Schedule: Al= -4,-3,-2,-1,0,1,2,3,4,6,8,10,12,16,20 deg

Table 4, Estimated Uncertainties

d. CONFIG BZU

0.4 0.55 0.8 0.95 1.05 1.1 0.0/0 0.060 0.038 0.034 0.032 0.031 0.029 0.025 0.015 0.014 0.013 0.013 0.039 0.034 0.022 0.019 0.019 0.019 0.020 0.017 0.011 0.0099 0.0095 0.0063 0.014 0.0076 0.0068 0.0065 0.0063 0.016 0.0040 0.0040 0.0043 0.0070 0.008 0.0086 0.0075 0.0032 0.0032	a il impada				Σ				
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0.029 0.025 0.015 0.014 0.013 0.013 0.039 0.034 0.022 0.020 0.019 0.019 0.032 0.028 0.016 0.015 0.015 0.020 0.017 0.011 0.0099 0.0096 0.0093 0.014 0.012 0.0076 0.0068 0.0065 0.0063 0.016 0.014 0.0086 0.0076 0.0073 0.0070 0.008 0.0086 0.0035 0.0032 0.0032	Z	0.00	090.0	0.038	0.034	0.032	0.031	0.030	0.029
0.039 0.034 0.022 0.020 0.019 0.019 0.032 0.028 0.018 0.016 0.015 0.015 0.020 0.017 0.011 0.0099 0.0096 0.0093 0.014 0.012 0.0076 0.0068 0.0065 0.0063 0.016 0.014 0.0086 0.0076 0.0073 0.0070 0.0088 0.0080 0.0035 0.0032 0.0032	CIM	0.029	0.025	0.015	0.014	0.013	0.013	0.012	0.012
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b. CONFIG B25

a 11 1WV aVa				Σ				
L VINVIAR I F. V.	0.4	0.55	8.0	96.0	1.05	1.1	1.2	1.3
S	0.0/3	0.063	0.039	0.035	0.033	0.032	0.030	0.029
WTO .	0.028	0.023	0.015	0.013	0.012	0.012	0.011	0.011
	0.039	0.034	0.022	0.020	0.019	0.018	0.018	0.017
CLN	0.032	0.028	0.018	0.016	0.015	0 015	0.014	0.014
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CAT	0.014	0.012	92000	0.0068	0.0065	0.0063	09000	0.0059
CA.	0.016	0.014	0.0086	9/00.0	0.0073	0.00.0	0.0067	0.0066
CAB	0.0088	0,0000	0.0041	0.0035	0.0032	0.0032	0.0030	0.0030

lable 4. Concluded

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c. CONFIG B30

0.4			Σ				
	0.55	8.0	96.0	1.05	1.1	1.2	1.3
CN 0.077	0.065	0.041	0.036	0.034	0.033	0.031	0.030
: !	0	0.014	0.012	0.012	0.011	0.011	0.010
	<u> </u>	0.022	0.020	0.019	0.018	0.018	0.017
:	0.028	0.018	0.016	0.015	0.015	0.014	0.014
<u> </u>	0	0.011	0.0099	0.0096	0.0093	0.0088	0.0086
<u> </u> 		0.0076	0.0068	0.0065	0.0063	0,0060	0.0059
i :	0.014	0.0086	0.0076	0.0073	0.0070	0.0067	0.0066
CAB 0.0088	0.0080	0.0041	0.0035	0.0032	0.0032	0.0030	0.0030

APPENDIX III

Sample Tabulated Data

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Sample 1. Body— and Stability—Axes Data	Sample 1. Body- and Stability-Axes Data	Π'	20.5	88	0	-0.133		88	200	0003	i		0.0102	0.4860	0.8010	-0.133	0.015	-8.899
-0.00 -0.1 0.015 0.0939 0.003 -0.0001 0.2255 0.2051 0.0164 0.5146 0.6187 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.003 0.003 0.003 0.0002 0.0001 0.0225 0.2051 0.0045 0.018 0.018 0.023 0.003 0.003 0.0002 0.0001 0.0002 0.0018 0.018 0.018 0.018 0.023 0.023 0.003 0.0003 0	8 Constant	'	0.02	88	- 0 0	0.00		88	0.000	-0.0003			0.0134	0.4953	0.7282	00.0	0.0	0.238
8 Sample 1. Body- and Stability-Axes Data	Sample 1. Body— and Stability—Axes Data		1.02	88	9	0.075		8 8	0000	000	- 1		0.0164	0.5146	0.6767	0.074	0.018	4. 198
9 -0.01 -0.1 0.281 0.186 0.004 0.0005 0.2100 0.0009 0.2009 0.0000	9 - 0.01 - 0.1 0 - 2391 0 - 0.00 0 - 0.000 0 - 0.200 0 - 0.200 0 - 0.000 0 -		2.98	9.0	9 9	0.213		98	0.002	0.00			0.0181	0.5045	0.6587	0.212	0.029	7.255
0.01 0.1 0.568 0.3879 0.003 0.0016 0.0004 0.2652 0.0014 0.5656 0.5656 0.065 1 -0.02 -0.1 0.746 0.5000 0.001 0.0016 0.0004 0.2422 0.0019 0.516 0.0319 0.142 0.0017 0.0019	8-0.05		4. n	000	,	0.281		9 8	0.0010	0.0002			0.0093	0.5035	0.6092	0.279	0.029	9.663
1 -0.02 -0.1 0.746 0.5003 0.001 0.0011 0.0006 0.2853 0.2956 0.5116 0.3293 0.1912 0.0007 0.0011 0.0012 0.0013 0.2956 0.5116 0.5019 1.3169 0.952 0.1047 0.003 0.0001 0.0016 0.003 0.0017 0.2031 0.0017 0.2037 0.0017 0.2037 0.0017 0.2037 0.0017 0.3244 0.1197 0.5399 0.8753 1.502 0.308 0.003 0.0037 0.0037 0.0017 0.3441 -0.1735 0.5452 0.9349 2.167 0.606 0.00504	1 -0.02 -0.1 0.746 0.5006 0.0010 0.00010 0.00006 0.2323 0.2956 0.0432 0.047 1 -0.03 -0.1 0.748 0.5009 0.0010 0.00010 0.2422 0.0991 -0.0669 0.5219 1.3169 0.952 0.134 1 -0.03 -0.1 1.529 0.6800 -0.004 0.0037 0.0017 0.2097 0.2094 -0.1197 0.5399 0.8753 1.502 0.308 1 -0.03 -0.1 2.244 1.1789 -0.003 0.0037 0.0017 0.2097 0.3394 -0.1195 0.5452 0.9349 2.167 0.606 2 CLW-AD Sample 1. Body- and Stability-Axes Data	ĺ	7.99	-0.01	-0	0.569		0.003	0.0015	0.0004	1		-0.0142	0.5051	0.5621	0.566	0.065	8.699
CLW-AD CLW-AD Sample 1. Body— and Stability—Axes Data	Sample 1. Body- and Stability-Axes Data	-1,	0.03	9	- 0	0.746		9.8	0.0011	0.0006	- 1		-0.0432	0.5116	0.3293	0.742	0.087	8.494
1 -0.03 -0.1 2.244 i.1789 -0.003 0.0037 0.0036 0.1707 0.3441 -0.1735 0.5452 0.9349 2.167 0.606 0.0604 0.0604	0.0504 CLW-AD CLW-AD O_0504 Sample 1. Body— and Stability—Axes Data		6.07	9 9	 - - - -	1.529		\$ 8 9 9	0.001	9.6			-0.0669 -0.1197	0.5399	0.8753	1.502	0.308	4.874
0.0504 0.0504 Sample 1. Body- and Stability-Axes	0.0504 Sample 1. Body- and Stability-Axes	14	0.03	-0.03	-0.1	2.244		-0.003	0.0037	0.0035	ı		-0.1735	0.5452	0.9349	2.167	909.0	3.578
Sample 1. Body- and Stability-Axes	Sample 1. Body- and Stability-Axes	10	1	CLM-A0 0.0504														
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TEST TC-793 S	SUMMARY 2								
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